



Model reduction: analysis, numerical solution and real world applications Lecture III: Model reduction in real world and industrial applications

Volker Mehrmann

TU Berlin, Institut für Mathematik

DFG Research Center MATHEON
Mathematics for key technologies



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- 1 Introduction**
- 2 Brake Squeal Model
- 3 Parameterized Model Reduction
- 4 Numerical Linear Algebra at Work
- 5 Adaptive Finite Elements for evp
- 6 Automated multilevel substructuring



Physical system



Modeling

Modeling



ODE/DAE

← *semidiscr.*

PDE



Mod. reduction



Reduced ODE/DAE



◀ ◻ ▶ *Sim., Control*





How to get a reduced order model depending on parameters?

- ▶ Semidiscretization in space using FV, FE, FD \implies large scale ODE/DAE-control problem (with parameters).
- ▶ Project on a subspace that captures the dynamics in a **large range of the parameters**.
- ▶ We can use all the methods as before, **survey by Benner, Gugercin, Willcox**, enriched by sampling of the parameter space.
- ▶ Reduced basis approach, books **A. Quarteroni, A. Manzoni, F. Negri, A. Quarteroni, G. Rozza**



Sparse representation of PDE solutions

Given PDE model that describes the space-time behavior.

- ▶ Numerical solution of PDE $Ly = f$, with differential operator L in a domain $\Omega \subset \mathbb{R}^d$ with boundary Γ and BC on Γ . **Data and solution depending on parameters (controls).**
- ▶ Let \mathcal{V} be an **ansatz function space** in which we know or expect the solution to be, **(depending on parameters, controls).**
- ▶ Choose another (or the same) space \mathcal{W} as **test space**.
- ▶ Classical Galerkin or Petrov-Galerkin approach: Seek solution y in some **finite dimensional ansatz space** $\mathcal{V}_n \subset \mathcal{V}$ (spanned by) $\mathcal{B} = \{\phi_1, \dots, \phi_n\}$, i.e. $y = \sum_{i=1}^n y_i \phi_i$ and $(Ly - f, w) = 0$ or $|(Ly - f, w)| < \epsilon$ for all $w \in \mathcal{W}$.

How sparse can we get?

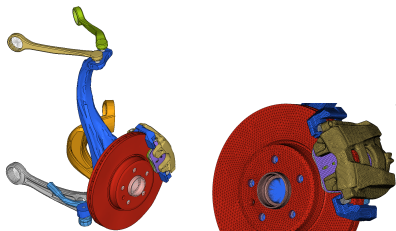


- ▶ What is a good space \mathcal{V} , so that y can be sparsely represented/approximated in \mathcal{V} (for a large parameter range)?
- ▶ Good space for forward or for optimization/control problem?
- ▶ What is a good basis of \mathcal{V}_n so that u can be sparsely represented/approximated.
- ▶ What are conditions for the basis so that the finite dimensional version $L_n y_n = f_n$ is easy to solve for many parameters?
- ▶ Is there a 'eierlegende Wollmilchsau', a swiss army knife?

Can only be answered for specific application.



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- ▷ Disc brake squeal is a frequent and annoying phenomenon (with cars, trains, bikes).
- ▷ Important for customer satisfaction, even if not a safety risk.
- ▷ **Nonlinear effect** that is hard to detect in experiments.
- ▷ The car industry is trying for decades to improve this, by changing the designs of brake and disc.

Can we do this model based?



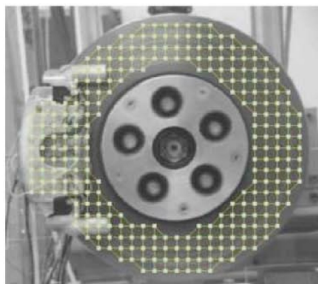
Interdisciplinary project with car manufacturers + SMEs

Supported by German Minist. of Economics via AIF foundation.

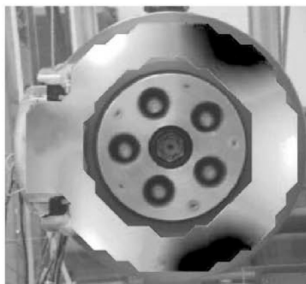
University: N. Gräbner, U. von Wagner, TU Berlin, Mechanics,
N. Hoffmann, TU Hamburg-Harburg, Mechanics,
S. Quraishi, C. Schröder, TU Berlin Mathematics.

Goals:

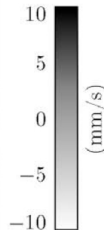
- ▶ Develop **model of brake system with all effects** that may cause squeal. (Friction, circulatory, gyroscopic effects, etc).
- ▶ **Simulate** brake behavior for **many different parameters** (disk speed, material geometry parameters).
- ▶ **Our task: Model reduction, solution of eigenvalue problems.**
- ▶ **Long term: Stability/bifurcation analysis for a given parameter region.**



Gitter der Messpunkte



Betriebsschwingform (1750 Hz)



1

- ▶ Experiments indicate nonlinear behavior (subcritical Hopf bifurcation) → film.

¹Institute f. Mechanics, TU Berlin



Atomistic scale: Many damped harmonic oscillators: **Langevin equation**.

$$m\ddot{q}(t) + d\dot{q}(t) + kq(t) = \xi(t),$$

- ▷ m mass, k stiffness.
- ▷ d describes damping and dissipation effects, (**very difficult to model in practice**).
- ▷ ξ is the Langevin complementary force random force, d and ξ are frequency dependent.

Not a good model for simulation and definitely not for optimization.

Errors and uncertainties very hard to quantify.



Multi-body system based on Finite Element Modeling (FEM)

- ▶ Write displacements of structure $z(x, t)$ as linear combination of basis functions (e.g. but not always piecewise polynomials),

$$z(x, t) \approx \sum_{i=1}^N q_i(t) \phi_i(x, t).$$

- ▶ Integrate against test functions (Petrov Galerkin) → **discretized model for the vibrations** in weak form.
- ▶ Add friction and damping as **macroscopic surrogate model** fitted from experimental data.
- ▶ **Simplifications**: Remove some nonlinearities, asymptotic analysis for small parameters, etc.
- ▶ **Produce reduced order model for large parameter set?**

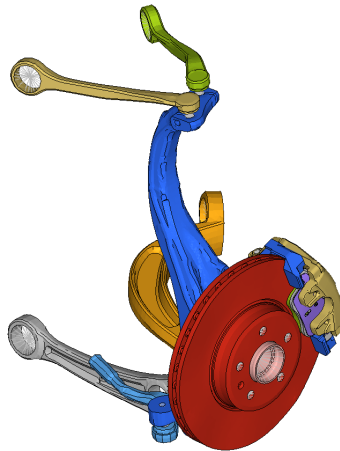
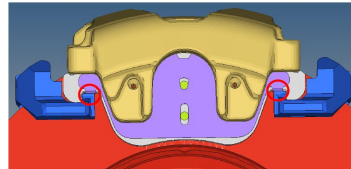
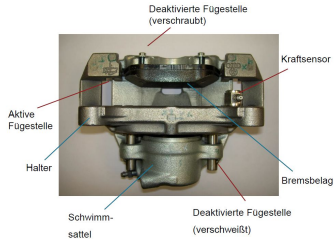


Figure: View of the brake model



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Figure: View of the brake model



Large differential-algebraic equation (DAE) system and evp
dep. on parameters (here only disk speed displayed).

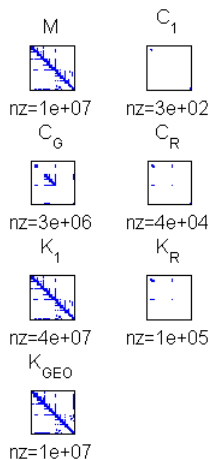
$$M\ddot{q} + \left(C_1 + \frac{\omega_r}{\omega} C_R + \frac{\omega}{\omega_r} C_G\right)\dot{q} + \left(K_1 + K_R + \left(\frac{\omega}{\omega_r}\right)^2 K_G\right)q = f,$$

- ▶ M symmetric, pos. semidef., **singular** matrix (constraints),
- ▶ C_1 symmetric matrix, material damping,
- ▶ C_G skew-symmetric matrix, gyroscopic effects,
- ▶ C_R symmetric matrix, friction induced damping, (phenomenological)
- ▶ K_1 symmetric stiffness matrix,
- ▶ K_R nonsymmetric matrix modeling circulatory effects,
- ▶ K_G symmetric geometric stiffness matrix.
- ▶ ω rotational speed of disk with reference velocity ω_r .



$$n = 842,638, \omega_r = 5, \omega = 17 \times 2\pi$$

matrix	pattern	2-norm	structural rank
M	symm	5e-2	842,623
C_1	symm	1e-19	160
C_G	skew	1.5e-1	217500
C_R	symm	7e-2	2120
K_1	symm	2e13	full
K_R	-	3e4	2110
K_G	symm	40	842,623





This is really a hierarchy and mixture of models.

- ▶ FE Model hierarchy: grid hierarchy, type of ansatz functions, component and domain decomposition.
- ▶ Coupled with surrogate model for friction and damping?

Challenges

- ▶ Are the simplifications: nonlinear/linear, expansion of small parameters justified?
- ▶ We do not really have a PDE, **error estimates, adaptivity?**
- ▶ **Parametric reduced model** for optimization, control, bifurcation analysis?
- ▶ Good subspace in function space or coordinate space?

This is a wave problem, eigenspaces seem a good choice.



- 1 Introduction
- 2 Brake Squeal Model
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- 4 Numerical Linear Algebra at Work
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- ▶ Ansatz $q(t) = e^{\lambda t} u$ gives a quadratic eigenvalue problem (QEP):

$$P_{\omega}(\lambda)u = (\lambda^2 M + \lambda C(\omega) + K(\omega))u = 0.$$

- ▶ Want evs with positive real part (**few, ideally one**, since squeal is **mono-frequent**) and corresponding evecs.
- ▶ Likelihood of a brake to squeal is correlated with **magnitude of positive real part** of eigenvalue.
- ▶ **Objective:** Efficient method to compute evs in right half plane for many parameter values e.g. $\omega \in (2\pi, 2\pi \times 20)$.



Determine subspace spanned by columns of matrix Q ,

- ▷ Project QEP: $P_\omega(\lambda)x = (\lambda^2 M + \lambda C(\omega) + K(\omega))x = 0$ or dynamical system into small d -dimensional subspace that is independent of ω .
- ▷ **projected QEP**
 - ▶ $\tilde{P}_\omega(\lambda) = Q^T P_\omega(\lambda) Q = \lambda^2 Q^T M Q + \lambda Q^T C(\omega) Q + Q^T K(\omega) Q$
- ▷ How to choose Q ?
 - ▶ **Sufficiently** accurate approximation of evs with positive real part
 - ▶ Ideally Q should contain good approximations to the desired evecs **for all parameter values**
 - ▶ One should be able to construct Q in a **reasonable amount of computing time**.



- ▶ Traditional approach to get a subspace Q :
 - ▶ Q_{TRAD} := dominant eigenvectors (i.e. eigenvectors with smallest eigenvalues) of generalized evp $L(\lambda) = (\mu M - K_1 - K_G)$
- ▶ Advantages:
 - ▶ One only has to solve a **large, sparse, symmetric, definite GEVP**.
- ▶ Disadvantages:
 - ▶ Subspace does not take into account damping and parameter dependence.
 - ▶ Often **poor approximation of evs/vecs of the full model**.



Use idea from proper orthogonal decomposition (POD) or dynamic mode decomposition (DMD).

- ▶ Compute matrices of evecs $X(\omega_i)$ corresponding to right half plane evs for full QEP $P_\omega(\lambda)x = 0$ and sample parameters $\omega_1, \omega_2, \dots, \omega_p$
- ▶ Construct measurement matrix $\tilde{X} = [X(\omega_1), X(\omega_2), X(\omega_3) \cdots X(\omega_p)]$ containing computed snapshot evecs.
- ▶ Extract **dominant directions** in \tilde{X} by a truncated singular value decomposition.

Same space can also be used with other approaches.



- 1 Introduction
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- 3 Parameterized Model Reduction
- 4 Numerical Linear Algebra at Work**
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Consider full problem $P_\omega(\lambda)x = 0$.

- ▶ Set $\lambda_\tau(\omega) = \lambda(\omega) - \tau$, where τ is such that $\det(P_\omega(\tau)) \neq 0$.
- ▶ New parametric QEP

$$P_{\omega,\tau}(\lambda(\omega))x(\omega) = (\lambda_\tau(\omega)^2 M_\tau + \lambda_\tau(\omega) C_\tau(\omega) + K_\tau(\omega))x(\omega) = 0,$$

where $M_\tau = M$, $C_\tau = 2\tau M + C$ and $K_\tau = \tau^2 M + \tau C + K$ is nonsingular.

- ▶ Shift point τ is chosen in the right half plane, ideally near the expected eigenvalue location.
- ▶ Consider reverse polynomial, then evs near τ become large in modulus, while evs far away from τ become small.



We use **classical companion linearization** (first order form)

$$A_\tau(\omega)v(\omega) = \mu_\tau B_\tau(\omega)v(\omega)$$

with

$$\begin{bmatrix} K_\tau(\omega) & 0 \\ 0 & I_n \end{bmatrix} \begin{bmatrix} v(\omega) \\ \mu_\tau(\omega)v(\omega) \end{bmatrix} = \mu_\tau(\omega) \begin{bmatrix} -C_\tau(\omega) & -M_\tau \\ I_n & 0 \end{bmatrix} \begin{bmatrix} v(\omega) \\ \mu_\tau v(\omega) \end{bmatrix}.$$



- ▶ Compute ev and evec approximations near shift τ via **shift-and-invert Arnoldi** method.
- ▶ Given $v_0 \in \mathbb{C}^n$ and $W \in \mathbb{C}^{n \times n}$, the **Krylov subspace** of \mathbb{C}^n of order k associated with W is

$$\mathcal{K}_k(W, v_0) = \text{span}\{v_0, Wv_0, W^2v_0, \dots, W^{k-1}v_0\}.$$

- ▶ Arnoldi obtains orthonormal basis V_k of this space and

$$WV_k = V_kH_k + fe_k^*,$$

- ▶ Columns of V_k approx. k -dim. invariant subspace of W .
- ▶ Evs of H_k approximate evs of W associated to V_k .
- ▶ Apply with shift τ and frequency ω to $W = B_\tau(\omega)^{-1}A_\tau(\omega)$.
Per step we multiply with $A_\tau(\omega)$ and solve system with $B_\tau(\omega)$.



- ▶ Construct **measurement matrix** $V \in \mathbb{R}^{n, km}$ containing 'unstable' evecs for a set of ω_i ,

$$V = [V(\omega_1), V(\omega_2), V(\omega_3), \dots, V(\omega_k)]$$

- ▶ Perform (partial) SVD $V = U\Sigma Z^H$

$$V = [\tilde{u}_1, \tilde{u}_2, \dots, \tilde{u}_{km}] \begin{bmatrix} \sigma_1 & & & & & \\ & \sigma_2 & & & & \\ & & \sigma_3 & & & \\ & & & \ddots & & \\ & & & & \sigma_{km} & \\ & & & & & \ddots \end{bmatrix} [\tilde{z}_1, \tilde{z}_2, \dots, \tilde{z}_{km}]^H$$

with U, Z unitary.



- ▶ Use approximation

$$\tilde{V} \approx [\tilde{u}_1, \tilde{u}_2, \dots, \tilde{u}_d] \begin{bmatrix} \sigma_1 & & & & & \\ & \sigma_2 & & & & \\ & & \sigma_3 & & & \\ & & & \ddots & & \\ & & & & \sigma_d & \\ & & & & & \ddots \end{bmatrix} [\tilde{z}_1, \tilde{z}_2, \dots, \tilde{z}_d]^H$$

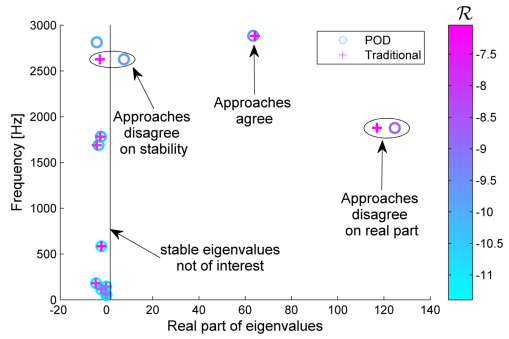
by deleting $\sigma_{d+1}, \sigma_{d+2}, \dots, \sigma_{km}$ that are small.

(Actually these are not even computed).

- ▶ Choose $Q = [\tilde{u}_1, \tilde{u}_2, \dots, \tilde{u}_d]$ to project $P_\omega(\lambda)$ or dynamical system.



Results real brake model





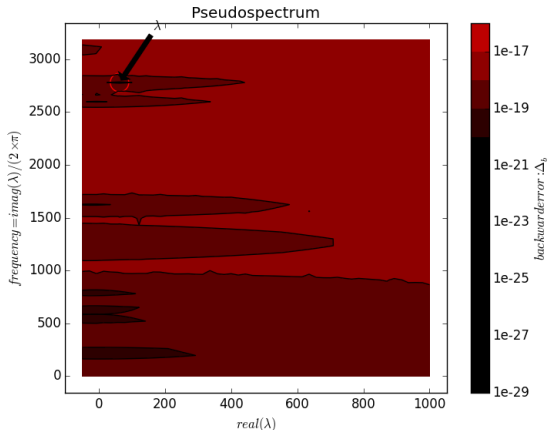
Do we believe we got have a good space?

- ▶ **Forward error**: $\Delta_f = |\lambda_{exact} - \lambda_{computed}|$
- ▶ **Backward error**: smallest in norm perturbation Δ_b to M, C, K such that $\tilde{v}, \tilde{\lambda}$ satisfies Q EVP defined by perturbed matrices $\tilde{M}, \tilde{C}, \tilde{K}$
- ▶ Computation of backward error: $\Delta_b(\lambda) = \frac{\|(\lambda^2 M + \lambda C + K)\|}{|\lambda|^2 \|M\| + |\lambda| \|C\| + \|K\|}$
- ▶ The **pseudospectrum** gives the level curves of $\Delta_b(\lambda)$.



Pseudospectrum of a toy brake model

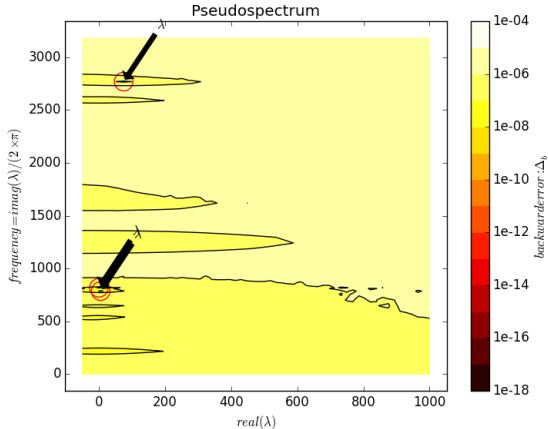
Brake model with 5000 dof, one of the springs had stiffness 10^{18} .





Pseudospectrum of a toy brake model

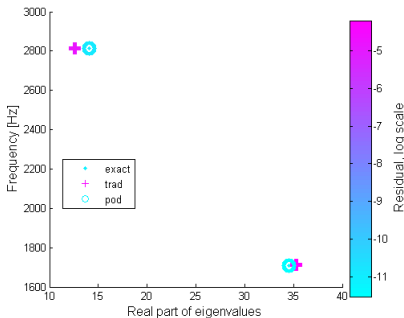
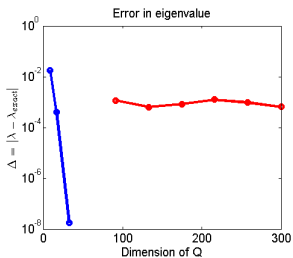
Brake model corrected with modeling high stiffness as rigid link.





Results with new POD method

Industrial model 1 million dof



▷ Solution for every ω

- ▶ Solution with 300 dimensional TRAD subspace \sim 30 sec
- ▶ Solution with 100 dimensional POD subspace \sim 10 sec



- ▶ New POD approach captures modal information better than traditional one, **but slower**.
- ▶ Current numerical linear algebra methods are not efficient (in particular those in commercially codes).
- ▶ Discrete FE and quasi-uniform grids followed by expensive model reduction **is really a waste**.
- ▶ Can we combine FE modeling and eigenvalue computation for modal truncation or other MOR methods?
- ▶ Can we get error estimates and adaptivity? (AFEM , AMLS).



- 1 Introduction
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Adaptive Finite Element Method

- ▶ Adaptive Finite Element methods refine the mesh where necessary, and coarsen where solution is well represented.
- ▶ They use a priori and a posteriori error estimators to get information about the discretization error.
- ▶ They are well established for PDE boundary value problems.
- ▶ **But here we want to use them for PDE eigenvalue problems, which is much harder.**
- ▶ And in the brake problem we do not have a PDE.
- ▶ Furthermore we have a parametric problem.



Solve → **Estimate** → **Mark** → **Refine**



Consider a model problem like the **disk brake without damping, gyroscopic, circulatory terms** and reasonable geometry.

$$\begin{aligned}\Delta u &= \lambda u && \text{in } \Omega \\ u &= 0 && \text{on } \partial\Omega\end{aligned}$$

This is just the traditional approach that is used in industry.
(Note $-\lambda^2$ in brake problem).



Weak formulation:

Determine ev/e.-function pair $(\lambda, u) \in \mathbb{R} \times V := \mathbb{R} \times H^1(\Omega; \mathbb{R})$ with $b(u, u) = 1$ and

$$a(u, v) = \lambda b(u, v) \quad \text{for all } v \in V,$$

where the bilinear forms $a(\cdot, \cdot)$ and $b(\cdot, \cdot)$ are defined by

$$a(u, v) := \int_{\Omega} \nabla u \cdot \nabla v \, dx, \quad b(u, v) := \int_{\Omega} uv \, dx \quad \text{for } u, v \in V.$$

Induced norms $\|\cdot\| := |\cdot|_{H^1(\Omega)}$ on V and $\|\cdot\| := \|\cdot\|_{L^2(\Omega)}$ on $L^2(\Omega)$.



Determine ev./e.-function pair $(\lambda_\ell, u_\ell) \in \mathbb{R} \times V_\ell$ with $b(u_\ell, u_\ell) = 1$ and

$$a(u_\ell, v_\ell) = \lambda_\ell b(u_\ell, v_\ell) \quad \text{for all } v_\ell \in V_\ell.$$

Use coordinate representation to get finite-dim. generalized evp

$$A_\ell x_\ell = \lambda_\ell B_\ell x_\ell$$

with stiffness matrix $A_\ell = [a(\varphi_i, \varphi_j)]_{i,j=1,\dots,N_\ell}$, mass matrix $B_\ell = [b(\varphi_i, \varphi_j)]_{i,j=1,\dots,N_\ell}$, in nodal basis $V_\ell = \{\varphi_1, \dots, \varphi_{N_\ell}\}$.

Discrete eigenvector: $x_\ell =: [x_{\ell,1}, \dots, x_{\ell,N_\ell}]^T$.

Approximated eigenfunction:

$$u_\ell = \sum_{k=1}^{N_\ell} x_{\ell,k} \varphi_k \in V_\ell.$$



This approach includes several errors:

- ▷ Model error (PDE model vs. Physics)
- ▷ Discretization error (finite dim. subspace)
- ▷ Error in eigenvalue solver (iterative method)
- ▷ Roundoff errors in finite arithmetic.

An error estimator η_ℓ is called *efficient and reliable* if there exist mesh-size independent constants C_{eff} C_{rel} such that

$$C_{\text{eff}}\eta_\ell \leq \|u - u_\ell\| \leq C_{\text{rel}}\eta_\ell.$$



Estimate the error a posteriori via

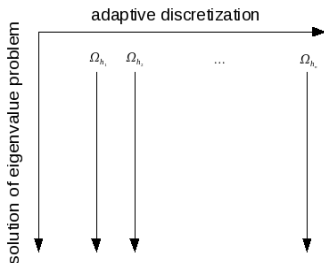
$$|\lambda - \lambda_\ell| + \|u - u_\ell\|^2 \lesssim \eta_\ell^2 := \|u_{\ell-1} - u_\ell\|^2.$$

Here \lesssim denotes an inequality that holds up to a multiplicative constant.

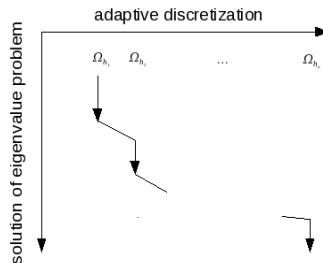
A posteriori error estimators for Laplace eigenvalue problem
Grubisic/Ovall 2009, M./Miedlar 2011, Neymeyr 2002



- ▷ Compute approx. eigenpair $(\tilde{\lambda}_H, \tilde{x}_H)$ on the coarse mesh,
- ▷ use iterative solver, i.e. Krylov subspace method,
- ▷ **but do not solve very accurately, stop after a few steps or when tolerance *tol* is reached.**
- ▷ Balance residual vector and error estimate **Miedlar 2011.**



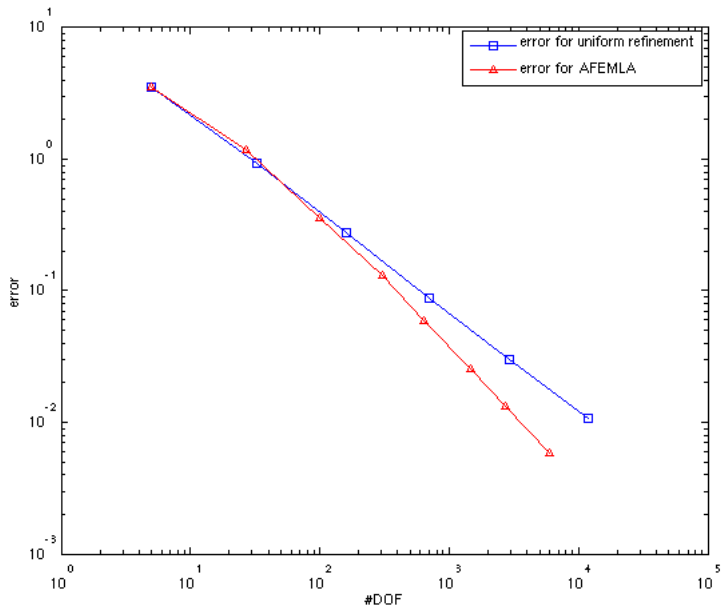
Standard AFEM



AFEMLA

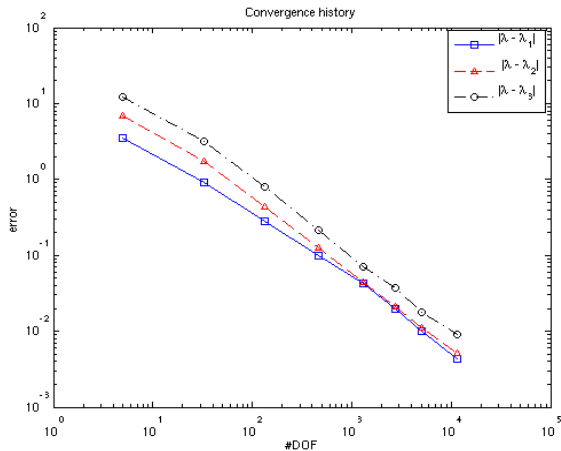


Conv. history AFEMLA





Conv. first 3 evs, L-shape domain.





Intermediate Conclusion

- ▶ For purely elliptic problems we can compute evs and efunctions very efficiently.
- ▶ Can be used to compute the subspace for the traditional approach.
- ▶ We have a priori/a posteriori error estimates which allow to adapt the mesh to the solution behavior.
- ▶ With the AFEMLA approach we can even work in a purely algebraic way if the underlying PDE is not available.
- ▶ It works also for several evs at a time (invariant subspaces).
- ▶ Proof of convergence **M./Miedlar 2011** if **saturation property** holds. Proof **Carstensen/Gedicke/M./Miedlar 2013**.
- ▶ So we can do the traditional approach also with adaptivity and tune in to the dominant evs.
- ▶ **But we want this for the full model.**



- ▶ Can we modify ideas for general problem?
- ▶ We need to deal with left and right evects, complex evs, Jordan blocks.
- ▶ What are the right spaces and norms?
- ▶ **Let us bring the nonsymmetry in via homotopy.**

$$\mathcal{H}(t) = (1 - t)\mathcal{L}_0 + t\mathcal{L}_1 \quad \text{for } t \in [0, 1],$$

where $\mathcal{L}_0 u := -\Delta u$.

Discrete homotopy for the model eigenvalue problem:

$$\mathcal{H}_\ell(t) = (\mathbf{A}_\ell + \mathbf{C}_\ell)(t) = (1 - t)\mathbf{A}_\ell + t(\mathbf{A}_\ell + \mathbf{C}_\ell) = \mathbf{A}_\ell + t\mathbf{C}_\ell.$$



A non-self-adjoint model problem

Carstensen/Gedicke/M./Miedlar 2012

Convection-diffusion eigenvalue problem:

$$-\Delta u + \gamma \cdot \nabla u = \lambda u \text{ in } \Omega \quad \text{and} \quad u = 0 \text{ on } \partial\Omega$$

Discrete weak primal and dual problem:

$$\begin{aligned} a(u_\ell, v_\ell) + c(u_\ell, v_\ell) &= \lambda_\ell b(u_\ell, v_\ell) \quad \text{for all } v_\ell \in V_\ell, \\ a(w_\ell, u_\ell^*) + c(w_\ell, u_\ell^*) &= \overline{\lambda_\ell^*} b(w_\ell, u_\ell^*) \quad \text{for all } w_\ell \in V_\ell. \end{aligned}$$

Generalized algebraic eigenvalue problem:

$$(A_\ell + C_\ell)u_\ell = \lambda_\ell B_\ell u_\ell \quad \text{and} \quad u_\ell^*(A_\ell + C_\ell) = \lambda_\ell^* u_\ell^* B_\ell$$

Smallest real part ev. is simple and well separated **Evans '00.**



Theorem (Carstensen/Gedicke/M./Miedlar 2012)

For model problem, the difference between the approx. ev. $\tilde{\lambda}_\ell(t)$ in the homotopy $\mathcal{H}_\ell(t)$ and the ev. $\lambda(1)$ of the original problem can be estimated via

$$\begin{aligned} \|\lambda(1) - \tilde{\lambda}_\ell(t)\| &\lesssim \nu(\tilde{\lambda}_\ell(t), \tilde{u}_\ell(t), \tilde{u}_\ell^*(t)) + \eta^2(\tilde{\lambda}_\ell(t), \tilde{u}_\ell(t), \tilde{u}_\ell^*(t)) \\ &\quad + \mu^2(\tilde{\lambda}_\ell(t), \tilde{u}_\ell(t), \tilde{u}_\ell^*(t)) \end{aligned}$$

in terms of

$$\begin{aligned} \nu(\tilde{\lambda}_\ell(t), \tilde{u}_\ell(t), \tilde{u}_\ell^*(t)) &:= (1-t)\|\gamma\|_\infty (\|\tilde{u}_\ell(t)\| + \|\tilde{u}_\ell^*(t)\|) \\ &+ (1-t)\|\gamma\|_\infty \left(\eta(\tilde{\lambda}_\ell(t), \tilde{u}_\ell(t), \tilde{u}_\ell^*(t)) + \mu(\tilde{\lambda}_\ell(t), \tilde{u}_\ell(t), \tilde{u}_\ell^*(t)) \right). \end{aligned}$$

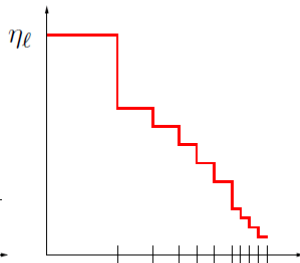
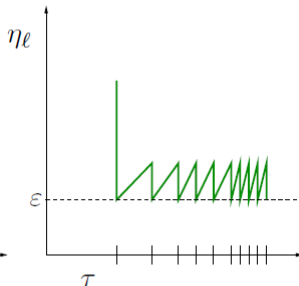
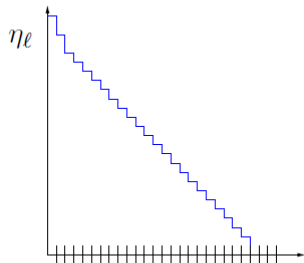


Adaptive homotopy algorithms

Algorithm 1: Balances the homotopy, discretization, iteration errors but uses fixed stepsize in homotopy.

Algorithm 2: Adaptivity in homotopy and iteration via stepsize control, discretization error is not decreased.

Algorithm 3: Adaptivity in the homotopy error, the discretization error, the iteration error including step size control.



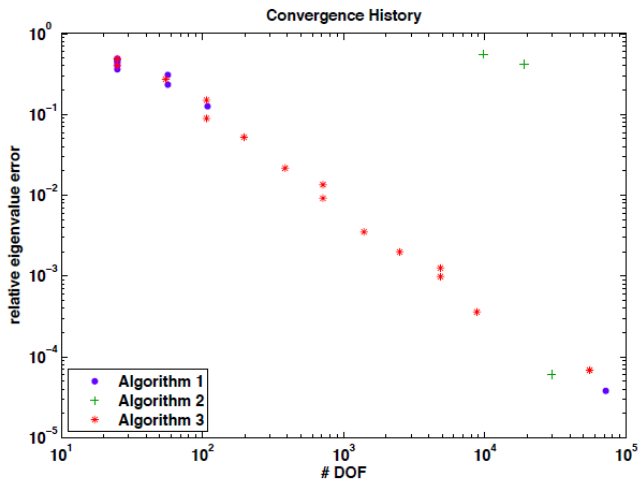


Figure: Conv. history of Algorithm 1, 2 and 3 with respect to #DOF.

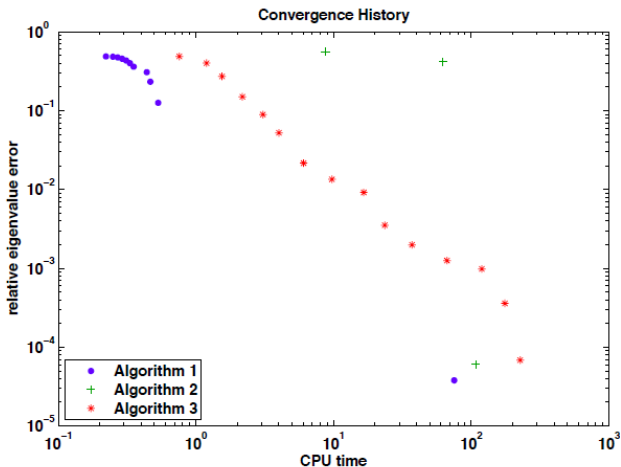


Figure: Conv. history of Algorithm 1, 2 and 3 with respect to CPU time.



- ▷ Extension of backward error analysis to PDE case **Miedlar 2011/2014**
- ▷ Error estimates for hp-finite elements for non-self-adjoint PDE evps **Giani/Grubisic/Miedlar/Ovall 2014**
- ▷ Multiple evs self-adjoint case **Galistil 2014**
- ▷ **No results on multiple, complex evs, Jordan blocks in non-self-adjoint case.**
- ▷ Highly oscillatory eigenfunctions can only be captured with fine grids.
- ▷ Can we enrich the ansatz space with these eigenfunctions?



- 1 Introduction
- 2 Brake Squeal Model
- 3 Parameterized Model Reduction
- 4 Numerical Linear Algebra at Work
- 5 Adaptive Finite Elements for evp
- 6 Automated multilevel substructuring**



Compute smallest evs of self-adjoint evp $(\lambda M - K)x = 0$ with M, K pos. def. as in traditional approach. **Bennighof-Lehouq 2004**

- Use symmetric reordering of matrix to block form or use directly domain decomposition partition. $(\lambda \tilde{M} - \tilde{K})x = 0$, with



structure

- Compute block Cholesky factorization of $\tilde{M} = LDL^T$ and form $\hat{K} = L^{-1}\tilde{K}L^{-T}$.
- Compute smallest evs and evecs of 'substructure' evps $(\lambda D_{ii} - \hat{K}_{ii})x_i$ and project large problem (modal truncation).
- Solve projected evp.



- ▶ This produces locally global (spectral) ansatz functions in substructure.
- ▶ This is a domain decomposition approach, where efunctions are used in substructures.
- ▶ Substructure efunctions are sparsely represented in FE basis.
- ▶ Analysis only for self-adjoint case and real simple evs.
- ▶ Works extremely well for mechanical structures with little damping.
- ▶ Does not work for brake problem.



- ▶ Using fine mesh and MOR usually works, but is a waste.
- ▶ Using evecs, efunctions or singular values can be combined with other MOR approaches.
- ▶ Error estimates are needed for non-self-adjoint case, multiple evs, complex evs, in combination with MOR methods.
- ▶ Enrich FEM ansatz space with approximate/substructure eigenfunctions?



- ▶ MOR is a topic to stay.
- ▶ Need to identify which problem we want to solve.
- ▶ Combination of adaptive FEM and AMLS type approaches with MOR methods.



**Thank you very much
for your attention.**



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