MORE Workshop September 6-10, 2015, Pilsen (Czech Republic)

Verification and effectivity of PGD model reduction

L. Chamoin, P. Ladevèze, P.E. Allier

LMT-Cachan (ENS Cachan / CNRS / Univ. Paris-Saclay) INRIA Rocquencourt - CERMICS

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Proper Generalized Decomposition Radial approximation Generalized spectral decomposition

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Outline

- Illustrations of PGD applications
- A posteriori error estimation: the CRE concept
- Control and adaptivity in PGD computations
- PGD performances and limits

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General ideas

[Chinesta *et al.* 2010, 2011]

Context: multiparameter EDPs (stochastic, optimization): *u*(*x, t, p*1*, p*2*,...,pn*)

- exponential growth of the number of dof with brute force approaches (curse of dimensionality)
- issues of computation cost / storage
- model order reduction: RB, POD, PGD,...

Idea of PGD: *a priori* representation using linear combination of modes with variable separation (tensor product space, low-rank structure, canonical format)

$$
u(x, t, p_1, p_2, \dots, p_n) \approx \sum_{m=1}^{M} \psi_m(x) \lambda_m(t) \phi_{1m}(p_1) \phi_{2m}(p_2) \dots \phi_{nm}(p_n)
$$

main features of the solution

- **The** *no* need of *a priori* information on the solution (no snapshot) decrease of computation/storage costs (linear growth of the number of dof)
- \rightarrow modes are computed offline and on the fly solving simple problems
- first used to solve NL time-dependent problems with LATIN [Ladeveze 99]
	- growing interest in the Computational Mechanics community

Computation of modes

.

When the **solution is known** (at least partially): an optimal low-rank separated representation may be searched by minimizing the distance with respect to a given metric on the tensor product

classical POD (SVD) approach with L2 norm and 2 variables

When the **solution is unknown**: several techniques (minimal residuals, (Petrov-) Galerkin formulation,...) [Nouy 2010]

we concentrate on progressive Galerkin-based method

.

$$
B(u, v) = L(v) \quad \forall v \qquad u_m = u_{m-1} + \psi(x)\lambda(t)\phi_1(p_1)\phi_2(p_2)\dots\phi_n(p_n)
$$

\n
$$
B(u_m, \psi^*\lambda\phi_1 \dots \phi_n) = L(\psi^*\lambda\phi_1 \dots \phi_n) \quad \forall \psi^* \longrightarrow \psi = F(\lambda, \phi_1, \dots, \phi_n)
$$

\n
$$
B(u_m, \psi\lambda^*\phi_1 \dots \phi_n) = L(\psi\lambda^*\phi_1 \dots \phi_n) \quad \forall \lambda^* \longrightarrow \lambda = G(\psi, \phi_1, \dots, \phi_n)
$$

\n
$$
B(u_m, \psi\lambda\phi_1^* \dots \phi_n) = L(\psi\lambda\phi_1^* \dots \phi_n) \quad \forall \phi_1^* \longrightarrow \phi_1 = J_1(\psi, \lambda, \phi_2, \dots, \phi_n)
$$

\n
$$
\vdots
$$

5 \rightarrow NL eigenvalue problem, solved with dedicated iterative strategies (fixed point) variants : convergence, mode orthogonalization, mode updating, ...

Transient thermal problem

LOt

$$
u = 0 \quad \text{on } \partial_u \Omega \times \mathcal{I}
$$

\n
$$
u_{|t=0} = 0
$$

\n
$$
\frac{\partial u}{\partial t} - \nabla \cdot \mathbf{q} = f_d
$$

\n
$$
\mathbf{q} \cdot \mathbf{n} = q_d \quad \text{on } \partial_q \Omega \times \mathcal{I}
$$

 $\mathbf{q} = k \nabla u$

Transient thermal problem

$$
u = 0 \text{ on } \partial_u \Omega \times \mathcal{I}
$$

\n
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u_{|t=0} = 0
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$$

 $q = k \nabla u$

multi-parameter problem : ${\bf x}, t, {\bf p}$

Transient thermal problem

L

$$
u = 0 \text{ on } \partial_u \Omega \times \mathcal{I}
$$

\n
$$
u_{|t=0} = 0
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\n
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$$

\n
$$
\mathbf{q} \cdot \mathbf{n} = q_d \text{ on } \partial_q \Omega \times \mathcal{I}
$$

\n
$$
\mathbf{q} = k \nabla u
$$

multi-parameter problem : x*, t,* p

Transient thermal problem

$$
u(\underline{x},t) \approx u_m(\underline{x},t) = \sum_{i=1}^m \psi_i(\underline{x}) \lambda_i(t) \longrightarrow m \times (N_h + N_{\Delta t})
$$
dot

«progressive Galerkin» approach

LOt

$$
u_m = u_{m-1} + \psi \lambda \quad \text{s.t.} \quad B(u_m, \psi^* \lambda + \psi \lambda^*) = L(\psi^* \lambda + \psi \lambda^*) \quad \forall \psi^*, \lambda^*
$$
\n
$$
B(u_m, \psi^* \lambda) = L(\psi^* \lambda) \quad \forall \psi^*
$$
\n
$$
B(u_m, \psi^* \lambda) = L(\psi^* \lambda) \quad \forall \psi^*
$$
\n
$$
B(u_m, \psi \lambda^*) = L(\psi \lambda^*) \quad \forall \lambda^*
$$
\n
$$
\alpha_T \frac{\lambda^{(k+1)} - \lambda^{(k)}}{\Delta t} + \beta_T \lambda^{(k)} = \delta_T^{(k)} \quad \lambda^{(0)} = 0
$$

- (guaranteed) estimation of the global/local error
- adaptivity criteria

Outline

- Basics on Proper Generalized Decomposition (PGD)
- Illustrations of PGD applications
- A posteriori error estimation: the CRE concept
- Control and adaptivity in PGD computations
- PGD performances and limits

model parameters are seen as extra-coordinates [Chinesta *et al.* 2011]

- **EXECUTE:** enables to address many engineering problems:
	- variations of material parameters
	- changes in boundary/initial conditions
	- changes in loading
	- geometry variations
	- data assimilation (PGD+Kalman filter) [Marchand *et al.* submitted]
	- PGD modes are computed offline and used online for inverse analysis, optimization with cheap and fast computations on light computing platforms
		- concept of virtual charts

Material parameters

 $q = k \nabla u$

Transient thermal problem

$$
u = 0 \quad \text{on } \partial_u \Omega \times \mathcal{I}
$$

\n
$$
u_{|t=0} = 0
$$

\n
$$
\frac{\partial u}{\partial t} - \nabla \cdot \mathbf{q} = f_d
$$

\n
$$
\mathbf{q} \cdot \mathbf{n} = q_d \quad \text{on } \partial_q \Omega \times \mathcal{I}
$$

multi-parameter problem : ${\bf x}, t, {\bf p}$

$$
B(u, v) = L(v) \quad \forall v \in H^1_{0, \Gamma_D}(\Omega) \otimes L^2(\mathcal{I}) \otimes_j L^2(\mathcal{P}_j)
$$

$$
B(u, v) = \int_{\Theta} \int_{\mathcal{I}} \int_{\Omega} (c \frac{\partial u}{\partial t} v + k \mathbf{\nabla} u \cdot \mathbf{\nabla} v) d\Omega dt d\mathbf{p}
$$

$$
L(v) = \int_{\Theta} \int_{\mathcal{I}} \left(\int_{\Omega} f_d v d\Omega + \int_{\Gamma_N} q_d v ds \right) dt d\mathbf{p}
$$

PGD modes

[Chamoin *et al* 2015]

- linear elastic material (small perturbations)
- $-$ extra-parameters: E (in each inclusion)

Geometry variations

■ Reference domain

■ Leading to an equivalent material

⚫ Use of Jacobian transformation

Geometry variations

■ Problem: heater

- convection on the top border
- ⚫ imposed flux on the bottom

Geometry variations

■ Problem: heater

- convection on the top border
- ⚫ imposed flux on the bottom

Nonlinear parametrized problems

APPRoFI project

- supported by the French National Research Agency
- collaboration between 7 industrials and academics
- **O** driven by SAFRAN

Problematic

- development of probabilistic approaches for the **robust design in fatigue**
- **taking into account variability** in durability simulations to guarantee the robustness and reliability of the design

Typical example

- \bullet blade of the Vulcain engine booster
- elasto-viscoplastic model
- variability of material properties
- variability of loadings

Engine blade

\blacksquare Description of the test-case

- ANR project APPROFI
- elasto-viscoplastic material

Parametric study

Parametric study

- **3 parameters: loading amplitude and material characteristics (Ro, Y)**
- \bigcirc 10 x 10 x 10 = 1,000 sets of parameters (range of variation $\pm 30\%$)
- \bullet influence on the maximum value of the σ_{miss}

Idea: to build a library of modes common to all sets using the LATIN solver

For a given set of parameters

Virtual chart

Parametric study

- \bullet 3 parameters: loading amplitude and material characteristics (R_0, Y)
- \bigcirc 10 x 10 x 10 = 1,000 sets of parameters (range of variation $\pm 30\%$)
- \bullet influence on the maximum value of the σ_{miss}

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Objectives

Goal: design a PGD algorithm such that:

- a given precision is attained
- as small as possible amount of computational work is needed

The designed error estimation method should:

- give a **fully computable upper bound** on the overall error (error control)
- enable to **distinguish** and **estimate** separately the **different error components**
- allow to **adjust optimally** the calculation parameters

Large litterature for error estimation and adaptive strategies (greedy) in reduced basis methods [Machiels *et al.* 2001, Grepl & Patera 2005,...]

specific case of PGD

- [Ladevèze 1998] *a priori* error estimation for separated variables representations (LATIN method)
- [Ammar *et al.* 2010] *a posteriori* error estimation for outputs of interest indicators based on residuals

[Moitinho de Almeida 2013] \longrightarrow goal-oriented error estimation using complementary solutions

Proposed estimate

PGD control, for linear elliptic or parabolic problems, with robust bounds [Allier *et al.* 2015, Ladevèze & L.C. 2011, 2012]

- → use of the Constitutive Relation Error (CRE) concept
	- widely used in the Computational Mechanics community for many years [Ladevèze & Leguillon 83, Destuynder & Métivet 99, Ladevèze & Pelle 04]
	- guaranteed and fully computable a posteriori error estimate on the energy norm method based on dual analysis, with recovery of equilibrated fluxes (verifying equilibrium in a strong sense) from the FEM solution
	- estimate split into several indicators to drive adaptive procedures

robust virtual charts that can be used for industrial design

 $-\nabla \cdot (k\nabla u) = f \text{ in } \Omega \text{ (equilibrium of flux } \mathbf{q} = k\nabla u$ $\mathcal K$: unif. bounded, strictly positive function $u = 0$ on Γ_D $k \nabla u \cdot \mathbf{n} = g \quad \text{on } \Gamma_N$ $f \in L^2(\Omega)$; $g \in L^2(\Gamma_N)$ *k*

Find
$$
u \in V
$$
 such that
 $a(u, v) = l(v) \quad \forall v \in V$

CONFORMING FEM

Find
$$
u_h \in V_h^p
$$
 such that
 $a(u_h, v_h) = l(v_h) \quad \forall v_h \in V_h^p$

$$
a(u, v) = \int_{\Omega} k \nabla u \cdot \nabla v d\Omega
$$

$$
l(v) = \int_{\Omega} f v d\Omega + \int_{\Gamma_N} g v ds
$$

$$
V = H_{\Gamma_D, 0}^1(\Omega)
$$

 $-\nabla \cdot (k\nabla u) = f \text{ in } \Omega \text{ (equilibrium of flux } \mathbf{q} = k\nabla u$ $\mathcal K$: unif. bounded, strictly positive function $u = 0$ on Γ_D $k \nabla u \cdot \mathbf{n} = g \quad \text{on } \Gamma_N$ $f \in L^2(\Omega)$; $g \in L^2(\Gamma_N)$ *k*

Find $u \in V$ such that $a(u, v) = l(v) \quad \forall v \in V$

CONFORMING FEM

Find
$$
u_h \in V_h^p
$$
 such that
 $a(u_h, v_h) = l(v_h) \quad \forall v_h \in V_h^p$

$$
a(u, v) = \int_{\Omega} k \nabla u \cdot \nabla v d\Omega
$$

\n
$$
l(v) = \int_{\Omega} fv d\Omega + \int_{\Gamma_N} g v ds
$$

\n
$$
V = H^1_{\Gamma_D, 0}(\Omega)
$$
 partition \overline{I}_h
\n
$$
V = H^1_{\Gamma_D, 0}(\Omega)
$$

discretization error $e = u - u_h$ global measure: $\sqrt{2}$ Ω k^{-1} • · • *d*Ω $|||e||| := \sqrt{a(e, e)} = |||{\bf q} - {\bf q}_h|||_q$

Space of equilibrated fluxes:

$$
W := \{ \mathbf{p} \in H(\text{div}, \Omega), \nabla \cdot \mathbf{p} + f = 0 \text{ in } \Omega, \mathbf{p} \cdot \mathbf{n} = g \text{ on } \partial_2 \Omega \}
$$

 $\int \mathbf{p} \cdot \nabla v d\mathbf{x} = \int f v d\mathbf{x} + \int g v d\mathbf{s} \quad \forall v \in H_{0,\partial_1\Omega}^1(\Omega)$ (weak form of equilibrium) Ω $\mathbf{p} \cdot \nabla v d\mathbf{x} =$:
: Ω $fvd\mathbf{x} +$:
: $\partial_2\Omega$ $g\nu d$ **s** $\forall \nu \in H^1_{0,\partial_1\Omega}(\Omega)$

 \rightarrow $\mathbf{p} \in W$ is said statically admissible (SA)

$$
J_2(\mathbf{q}) = \min_{\mathbf{p} \in W} J_2(\mathbf{p}) \quad ; \quad J_2(\mathbf{p}) := \frac{1}{2} \int_{\Omega} k^{-1} \mathbf{p} \cdot \mathbf{p} d\mathbf{x}
$$

For any approximation \hat{u}_h of u which is kinematically admissible (KA), we define: $(\hat{u}_h \in H^1(\Omega) \; ; \; \hat{u}_h|_{\partial_1 \Omega} = 0)$ flux field p which is SA

CRE functional

$$
E_{CRE}^2(\hat{u}_h, \mathbf{p}) := \int_{\Omega} k^{-1} (\mathbf{p} - k \nabla \hat{u}_h)^2 d\mathbf{x} \equiv |||\mathbf{p} - k \nabla \hat{u}_h|||_{\mathcal{F}}^2 = 2(J_1(\hat{u}_h) + J_2(\mathbf{p}))
$$

 $|||u - \hat{u}_h||| = E_{CRE}(\hat{u}_h, \mathbf{q}) \leq E_{CRE}(\hat{u}_h, \mathbf{p}) \quad \forall \mathbf{p} \in W$ ₂₆

Properties

- Prager-Synge equality:
	- $|||u \hat{u}_h|||^2 + |||\mathbf{q} \mathbf{p}|||^2_{\mathcal{F}} = E^2_{CRE}(\hat{u}_h, \mathbf{p}) \quad \forall \mathbf{p} \in W$
		- easily obtained from ! Ω $(\mathbf{q} - \mathbf{p}) \cdot \mathbf{\nabla} (u - \hat{u}_h) d\mathbf{x} = 0$
- Hypercircle equality:

$$
4|||\mathbf{q} - \mathbf{p}^*|||^2_{\mathcal{F}} = E_{CRE}^2(\hat{u}_h, \mathbf{p}) \quad \forall \mathbf{p} \in W
$$

with
$$
\mathbf{p}^* = \frac{1}{2}(\mathbf{p} + k \nabla \hat{u}_h)
$$

- used for goal-oriented error estimation
- Technical point: construction of a relevant admissible flux q ˆ *^h* ∈ *W*
	- post-processing of the approximate solution u_h (use of Galerkin properties in the FE context no full dual computation)
		- [Ladevèze & Leguillon 83, Destuynder & Métivet 99, Vohralik 12, Pares & Diez 06 Pled *et al.* 11,12]

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provides for asymptotic convergence properties [Ladevèze & Pelle 2004] $|||u - u_h||| \le E_{CRE}(u_h, \hat{q}_h) \le C|||u - u_h||$

Construction of hub of the main rotor which is used as a coupling sleeve between the helicopter frame and the rotor system. The structure is clamped at one end and subjected to a unit traction force density *t*, normal to the surface, on the other end. Let \mathcal{L} \mathbf{v} and the structure of \mathbf{q} p elements and 5898 nodes (i.e. 1794 degrees of freedom), are shown in Figure 23. The reference $\hat{\mathbf{q}}_h$

K

i

osition)[Ladevèze 75, Ladevèze et al 10] **Hybrid approach (domain decomposition)**[Ladevèze 75, Ladevèze et al 10]

 $\hat{a}_{11} = \hat{a}_{12} - \hat{a}_{12}$ and comparison \hat{a}_{11} **Step 1** : construction of equilibrated tractions $\hat{g}_K = \sigma_K \hat{g}_\gamma$ on element edges γ is not a design zone. Conversely, the selected region in $\mathbf x$ plays and $\mathbf x$

$$
\int_K f d\Omega + \int_{\partial K} \hat{g}_K ds = 0 \quad \forall K \quad ; \quad \hat{g}_K = g \quad \text{on } \Gamma_N \quad \left\{\right\}
$$

$$
\sum_{i} \text{condition} \int_{\partial K} \hat{g}_K \varphi_i ds = \int_K (\mathbf{q}_h \cdot \nabla \varphi_i - f \varphi_i) d\Omega = Q_i^K
$$

K

elements and $\frac{1}{2}$ nodes (i.e. 1794 degrees of $\hat{\alpha}$ **Dued Z** : local construction of **U** μ is a **Step 2** : local construction of $\hat{q}_{h|K}$ at the element level, verifying: $\overline{1}$ $\overline{1}$ $\overline{2}$ $\overline{1}$ $\overline{2}$ $\overline{1}$ $\overline{$ $\mathbf{v} - \mathbf{v} \cdot \mathbf{0}$ in the total corresponds to the corresponds t is not a design $\mathbf{L}[t] \mathbf{I}$ \mathbf{L} plays and \mathbf{L} in Figure 24 plays and \mathbf{L} $-\nabla \cdot \hat{\mathbf{q}}_{h|K} = f \text{ in } K \text{ ; } \hat{\mathbf{q}}_{h|K} \cdot \mathbf{n}_K = \hat{g}_K \text{ on } \partial K$ *h|K*

Figure 23. Hub model problem (left) and associated FE mesh (right). Orange plans represent clamped plans represent clamped \mathcal{L} solved using PGD (offline) reference solution

implemented in a C++ plateform

design purposes and engineering interest. The FE stress field in the selected region is depicted in Figure 24 and the admissible stress fields obtained from the three techniques are displayed in

Figure 25.

Extension of CRE

Definition in the unsteady case

$$
E_{CRE}^2(u_h, \hat{\mathbf{q}}_h) = |||\hat{\mathbf{q}}_h - k\nabla u_h|||_q^2 \qquad \int_0^T \int_{\Omega} k^{-1} \cdot \cdot d\Omega dt
$$

Fundamental result

$$
|||u - u_h|||^2 + |||q - \hat{q}_h|||^2_q + \int_{\Omega} c(u - u_h)|^2_T d\Omega = E_{CRE}^2(u_h, \hat{q}_h)
$$

guaranteed bounding on global and local errors

Rem : can be generalized to time-dependent nonlinear problems with dissipation

dissipation error [Ladevèze & Moës 98, Chamoin *et al.* 07]

$$
e_{dis}^2(\dot{X}, Y) = \varphi(\dot{X}) + \varphi^*(Y) - \dot{X} \cdot Y
$$

 \setminus

convex pseudo-potentials (with Fenchel's duality)

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Use of the CRE concept

Example: thermal problem solved with PGD

 $u_m(\mathbf{x}, t, k, c) = \sum \psi_i(\mathbf{x}) \lambda_i(t) f_i(k) g_i(c)$; $\mathbf{q}(u_m) = k \nabla u_m$ *m* $i=1$

- \hat{u} should be compatible (KA) : $\hat{u} = 0$ on $\Gamma_D \times \mathcal{I}$; $\hat{u}_{|t=0} = 0 \quad \forall \mathbf{p}$ we choose $\hat{u} = u_m$
- $(u_m, \mathbf{q}(u_m))$ is not SA in a FE sense \bullet (\hat{u}, \hat{q}) should be equilibrated (SA) : then, use of classical FE techniques (prolongation condition) necessary to post-process to get (u_m, \mathbf{q}_m) SA in a FE sense !
!
! Ω $\hat{\mathbf{q}} \cdot \mathbf{\nabla} u^* d\Omega =$!
! Ω $(f_d - c)$ $\partial \hat{u}$ ∂*t* $\int u^*d\Omega +$!
! Γ_N $q_d u^* ds$ $\forall u^* \in V, \forall t, \forall p$

32

We stop PGD sub-iterations with a problem in space

for each PGD mode $m_0 \in [1, m]$

$$
B(u_{m_0}, \psi^* \lambda_{m_0} \Gamma_{m_0}) = L(\psi^* \lambda_{m_0} \Gamma_{m_0}) \quad \forall \psi^* \in \mathcal{V}_h
$$

assumption: radial loading
$$
f_d = \sum_{j=1}^{J} \alpha_j(t) f_d^j(\mathbf{x}) \qquad q_d = \sum_{j=1}^{J} \beta_j(t) q_d^j(\mathbf{x})
$$

\n**Q**₀ =
$$
\sum_{j=1}^{J} \left[\alpha_j(t) q_{0,f}^j(\mathbf{x}) + \beta_j(t) q_{0,q}^j(\mathbf{x}) \right]
$$

\nis equilibrated in a FE sense with (f_d, q_d) , for all t

\n**Q**_{m₀}

\n**Q**_{m₀}

\n
$$
A_{m_0 i}
$$

\n
$$
\int_{\Omega} \left(\int_{\Theta} \int_{\mathcal{I}} \lambda_{m_0} \Gamma_{m_0}(k \nabla u_{m_0} - \mathbf{q}_0) dt d\mathbf{p} \right) \cdot \nabla \psi^* d\Omega + \int_{\Omega} \sum_{i=1}^{m_0} \left[\int_{\Theta} \int_{\mathcal{I}} c \lambda_{m_0} \Gamma_{m_0} \lambda_i dt d\mathbf{p} \right] \psi_i \psi^* d\Omega = 0 \quad \forall \psi^* \in V_n
$$

Post-processing

$$
\int_{\Omega} \mathbf{A} \Psi_{m} \psi^{*} d\Omega + \int_{\Omega} \{\mathbf{Q}\}_{1}^{m} \cdot \nabla \psi^{*} d\Omega = 0 \quad \forall \psi^{*} \in V_{h}
$$
\n
$$
\int_{\Omega} \Psi_{m} \psi^{*} d\Omega + \int_{\Omega} \mathbf{A}^{-1} \{\mathbf{Q}\}_{1}^{m} \cdot \nabla \psi^{*} d\Omega = 0 \quad \forall \psi^{*} \in V_{h}
$$
\n
$$
\int_{\Omega} c \mathbf{\Gamma}_{m} \otimes \mathbf{\Lambda}_{m} \otimes \Psi_{m} \psi^{*} d\Omega + \int_{\Omega} c \mathbf{\Gamma}_{m} \otimes \mathbf{\Lambda}_{m} \otimes \mathbf{A}^{-1} \{\mathbf{Q}\}_{1}^{m} \cdot \nabla \psi^{*} d\Omega = 0 \quad \forall \psi^{*} \in V_{h}, \forall t, \forall p
$$
\n
$$
\mathbf{\dot{u}}_{m}
$$
\n
$$
(u_{m}, \mathbf{\bar{q}}_{m} + \mathbf{q}_{0}) \text{ satisfies FE equilibration}
$$

we construct a SA field following the standard procedure

$$
\hat{\mathbf{q}}_m = \mathbf{q}_0 - c\mathbf{\Gamma}_m \otimes \dot{\mathbf{\Lambda}}_m \otimes \mathbb{A}^{-1} \{\hat{\mathbf{Q}}\}_1^m
$$

CRE estimate

 \blacktriangleright convergence for $m = 3$

asymptotic value = discretization error

Splitting of error sources

$$
u^{ex} - u_m^{h,\Delta t} = (u^{ex} - u^{h,\Delta t}) + (u^{h,\Delta t} - u_m^{h,\Delta t})
$$

\n
$$
\underbrace{||[u^{ex} - u_m^{h,\Delta t}||]_u^2}_{\text{total error}} = \underbrace{||[u^{h,\Delta t} - u_m^{h,\Delta t}||]_u^2}_{\text{PGD truncation error}} + \underbrace{||[u^{ex} - u^{h,\Delta t}||]_u^2}_{\text{discretization error}}
$$

\nestimated with a discretized reference model
\npost-processing of (u_m, \mathbf{q}_m) to get an admissible solution $(\hat{u}^{h,\Delta t}, \hat{\mathbf{q}}^{h,\Delta t})$
\nin the sense of the new reference problem (weaker sense in space and time)
\n
$$
\hat{q}^{h,\Delta t} = \mathbf{N}^T [\int_0^T \mathbf{N}^T \mathbf{N} dt]^{-1} [\mathbf{R}_1, \dots, \mathbf{R}_k]}
$$
\n
$$
\mathbf{E}_{CRE,PGD} = ||[\hat{\mathbf{q}}^{h,\Delta t} - k \nabla \hat{u}^{h,\Delta t}||]_q
$$
\n
$$
\mathbf{E}_{CRE,dis} = \sqrt{E_{CRE}^2 - E_{CRE,PGD}^2}
$$
\n35

Splitting of error sources

Possible to split space/time discretization errors

$$
E_{CRE,dis}^2 = E_{CRE,h}^2 + E_{CRE,\Delta t}^2
$$

$$
\|\hat{\mathbf{q}} - \hat{\mathbf{q}}^h\|_q \quad \|\hat{\mathbf{q}}^h - \hat{\mathbf{q}}^{h,\Delta t}\|_q
$$

discretization error in space : 83%

IDEA : the model is adapted mode after mode by comparing contributions of error sources (greedy algorithm)

- first PGD modes give general aspects : coarse approximation is sufficient
- next modes need more accuracy : fine discretization required

Error on a QoI

An optimal PGD decomposition for u_m is usually not optimal for $I(u_m)$

use of goal-oriented techniques

solution \tilde{u} = **influence function** (impact of global error on local error)

Goal-oriented error estimation

From an admissible solution $(\hat{\tilde{u}}, \hat{\tilde{q}})$ optimized bounding possible [Chamoin *et a*l 08, Pled *et al* 12] $I(u) - I(u_m) = \int_{0}^{T}$ 0 :
1970 - Paul Barnett, amerikanischer Paul Barnett, amerikanischer Paul Barnett, amerikanischer Paul Barnett,
1970 - Paul Barnett, amerikanischer Paul Barnett, amerikanischer Paul Barnett, amerikanischer Paul Barnett, a Ω $\sqrt{ }$ *c* $\partial(u-u_m)$ ∂*t* \widetilde{u} $\hat{\tilde{u}} + \boldsymbol{\nabla} (u - u_m) \cdot \hat{\tilde{\mathbf{q}}}$ \mathbf{A} *d*Ω*dt* = \int_0^T 0 :
11 Ω $k^{-1}(\mathbf{q} - \hat{\mathbf{q}})(\hat{\mathbf{q}} - k\boldsymbol{\nabla}\hat{\tilde{u}})d\Omega dt + I_{corr}(\hat{\mathbf{q}}, \hat{\tilde{\mathbf{q}}})$ $|I(u) - I(u_m) - I_{corr}(\hat{\bf q}, \tilde{\bf q})|$ $|\hat{\tilde{\mathbf{q}}})| \leq E_{CRE} \times \tilde{E}_{CRE}$

Sources splitting

$$
I(u^{ex}) - I(u^{h,\Delta t}_{m}) = \underbrace{[I(u^{ex}) - I(u^{h,\Delta t})] + [I(u^{h,\Delta t}) - I(u^{h,\Delta t}_{m})]}_{\square}
$$

discretization error

discretization error PGD truncation error

Solving the adjoint problem

Goal-Oriented Error Estimation

From adjoint-based techniques + CRE properties

~ m

$$
|I_{ex}(\mathbf{p}) - I_m(\mathbf{p}) - I_{corr}(\mathbf{p})| \leq E_{CRE}(\mathbf{p}) \cdot \tilde{E}_{CRE}(\mathbf{p})
$$

$$
I^-(\mathbf{p}) \leq I_{ex}(\mathbf{p}) \leq I^+(\mathbf{p})
$$

Sources splitting

$$
I_{ex} - I_{m}^{h, \Delta t} = [I_{ex} - I_{m}^{h, \Delta t}] + [I_{m}^{h, \Delta t} - I_{m}^{h, \Delta t}]
$$

\ndiscretization error
\n
$$
I = \sup_{k, c} \frac{1}{\omega} \int_{\omega} u_{T} d\omega
$$

\ndiscretized reference model
\n
$$
I = \sup_{k, c} \frac{1}{\omega} \int_{\omega} u_{T} d\omega
$$

- first PGD modes give general aspects : coarse approximation is sufficient
- next modes need more accuracy : fine discretization required

Guaranteed virtual chart

$$
I(k,c)=_{\omega,T}
$$

LOt

Outline

- Illustrations of PGD applications
- A posteriori error estimation: the CRE concept
- Control and adaptivity in PGD computations
- PGD performances and limits

Idelsohn's benchmark

 $c \frac{\partial u}{\partial t}(x,t) - \frac{\partial \sigma}{\partial x}(x,t) = \delta(x - vt)$

 $u(0,t) = u(L,t) = 0$

 $u(x, 0) = 0$

 $\sqrt{ }$

 \int

 \overline{a}

Reference solution

TAST

● brute force FEM solution

c, *k*

- SVD decomposition according to energy norm
- Θ optimal one

Reference reduction error

● neglect the discretization error

$$
\overline{e_{ref}} = \frac{\|u_h - u_m\|_E}{\|u_h\|_E}
$$

Idelsohn's benchmark

 $\int_{0}^{\infty} \frac{\partial t}{\partial \Omega}$ $\sqrt{ }$ \int \overline{a} $c \frac{\partial u}{\partial t}(x,t) - \frac{\partial \sigma}{\partial x}(x,t) = \delta(x - vt)$ $u(0,t) = u(L,t) = 0$ $u(x, 0) = 0$

Reference solution

SSI

- **brute force FEM solution**
- SVD decomposition according to energy norm
- Θ optimal one

Reference reduction error

O neglect the discretization error

$$
\overline{e_{ref}} = \frac{\|u_h - u_m\|_E}{\|u_h\|_E}
$$

Convergence of PGD strategies

Update of time fonctions (LMT method)

Minimal CRE in PGD

[Allier *et al* 2015]

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Idea

- Minimizing the CRE indicator: $\argmin_{u \in \mathcal{T}} \| e_{CRE}(u, \sigma) \|_E$
- Under the condition of equilibrium (**without the constitutive relation**) *u,*σ

$$
B(u, \sigma; v) = L(v) \quad \forall v \in \mathcal{V} \otimes \mathcal{T}
$$

Advantages

- \odot Immediate reduction error estimator;
- **Pilots the progressive algorithm;**
- Easy access to full error estimator through classical FEM CRE methods.

Minimisation

- partial
- full

Estimation through CRE

Only an estimation !

$$
\overline{e_{CRE}} = \frac{\|\tau_m - \mu \frac{\partial u_m}{\partial x}\|_E}{\|\tau_m + \mu \frac{\partial u_m}{\partial x}\|_E}
$$

Minimisation of CRE

Update of time fonctions (LMT method)

Effectivity of CRE indicator

Lifting

- with the solution of infinity domain: y
s
- with space limit conditions:

Galerkin PGD method for cor

Is the exact solution separable ? *c*, *k*

Is the exact solution separable ?

Influence of the instationnary term (v=L/T)

 \odot targeted error: 10⁻²

Conclusions and prospects

PGD model reduction

- ⚫ a priori construction of modes
- explicit solution with respect to parameters
- offline/online strategy
- variable separation should be driven by the physics of the problem

Error estimation for PGD reduced models

- separates the sources of the error
- allows adaptative PGD procedure
- ⚫ guaranteed bounds (robust virtual charts)

In progress

- extension to space separation: $u \approx \sum$ *m* $\psi_i(x)\gamma_i(y)\lambda_i(z)$
- ⚫ error estimation in the non-linear case (through LATIN method) *i*=1

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